## DEPARTMENT OF HEALTH CARE ACCESS AND INFORMATION FACILITIES DEVELOPMENT DIVISION

## APPLICATION FOR HCAI PREAPPROVAL OF MANUFACTURER'S CERTIFICATION (OPM)

HCAI Preapproval of Manufacturer's Certification (OPM)
Type: $\square$ New $\square$ Renewal/Update

## Manufacturer Information

Manufacturer: BD Integrated Diagnostics Solutions
Manufacturer's Technical Representative: Mathew Mellarkey
Mailing Address: 7 Loveton Circle, Sparks, MD 21152
Telephone: (410) 316-4810 Email: Mathew.Mellarkey@bd.com

## Product Information

Product Name: TOTALYS MULTIPROCESSOR
Product Type: Cytology Sampler
Product Model Number: Totalys Multiprocessor
General Description: Analysis samples for cervical cancer

## Applicant Information

Applicant Company Name: CYS Structural Engineers, Inc.
Contact Person: Dieter Siebald
Mailing Address: 2495 Natomas Park Drive, Suite 650, Sacramento, CA 95833
Telephone: (916) 920-2020 Email: dieters@cyseng.com
Title: Structural Engineer

STATE OF CALIFORNIA - HEALTH AND HUMAN SERVICES AGENCY

## Registered Design Professonal Preparing Engineering Recommendations

Company Name: CYS STRUCTURAL ENGINEERS, INC.
Name: Dieter Siebald California License Number: S4346
Mailing Address: 2495 Natomas Park Drive, Suite 650, Sacramento, CA 95833
Telephone: (916) 920-2020 Email: dieters@cyseng.com

## HCAI Special Seismic Certification Preapproval (OSP)

Special Seismic Certification is preapproved under OSP
OSP Number:

## Certification Method

Testing in accordance with: $\square$ ICC-ES AC156 $\square$ FM 1950-16
$\square$ Other(s) (Please Specify):

*Use of criteria other than those adopted by the California Building Standards Code, 2019 (CBSC 2019) for component supports and attachments are not permitted. For distribution system, interior partition wall, and suspended ceiling seismic bracings, test criteria other than those adopted in the CBSC 2019,may be used when approved by HCAI prior to testing.

X Analysis
$\square$ Experience Data

$\square$ Combination of Testing, Analysis, and/or Experience Data (Please Specify): $\qquad$

## HCAI Approval

Date: 5/18/2022
Name: William Staehlin
Title: Senior Structural Engineer
Condition of Approval (if applicable):
"Access to Safe, Quality Healthcare Environments that Meet California's Diverse and Dynamic Needs"
STATE OF CALIFORNIA - HEALTH AND HUMAN SERVICES AGENCY

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CYS STRUCTURAL ENGINEERS, INC.
2495 NATOMAS PARK DRIVE, SUITE 650
SACRAMENTO, CA 95833
TEL (916) 920-2020

| Job No: | 22018.02 |
| :--- | :--- |
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## GENERAL NOTES:

1. THIS HCAI PRE-APPROVAL OF MANUFACTURER'S CERTIFICATION (OPM) IS BASED ON THE CBC 2019. THE DEMAND (DESIGN FORCES) FOR USE W/ THIS OPM SHALL BE BASED ON THE CBC 2019.
2. IT IS THE RESPONSIBILITY OF THE SEOR FOR A SITE SPECIFIC PROJECT TO VERIFY:
A. THE ADEQUACY OF THE NEW OR EXISTING STRUCTURE TO RESIST THE FORCES \& WT SPECIFIED FOR EA EQUIP IN ADDITION TO ALL OTHER LOADS. PROVIDE \& DESIGN SUPPLEMENTARY MEMBERS AS REQ.
B. THAT THE FLR ANCHORS ARE LOCATED AT AN ADEQUATE DISTANCE FROM ANY SLAB EDGES OR OPGS.
C. THAT THE FLR ANCHORS ARE LOCATED AT AN ADEQUATE DISTANCE FROM ANY NEW OR EXISTING anchors. THE SPCG SHOWN IN THE TEST TORQUE TABLE BLW IS THE REQ MIN SPCG OF THE GIVEN DIA ANCHORS. THE REQ SPCG FROM ANCHORS OF OTHER DIAMETERS \& EMBEDMENTS MAY VARY \& SHALL BE EVALUATED BY THE SEOR.
D. THAT THE INSTALLATION IS IN CONFORMANCE W/ THE CBC 2019 \& W/ THE DETAILS SHOWN IN THIS PRE-APPROVAL.
E. THAT THE ACTUAL EQUIP'S WT, CENTER OF GRAVITY (CG) LOCATION, ANCHOR LOCATIONS, ANCHOR DETAILS, \& THE MATERIAL \& GAUGE OF THE EQUIP WHERE ATTACHMENTS ARE MADE, AGREE W/ THE INFO SHOWN ON THE PRE-APPROVAL DOCUMENTS.
F. THAT THE PROJECT SPECIFIC VALUES OF Sos $\& z / h$ RESULT IN SEISMIC FORCES THAT DO NOT EXCEED THE VALUES IN THE DESIGN CRITERIA.
3. EXPANSION ANCHORS INSTALLED IN NWC OR SLWC SHALL BE CARBON STL HILTI KB-TZ OR HILTI KB-TZ2 EXPANSION ANCHORS AS NOTED COMPLYING W/ ESR-1917 REISSUED MAY 2021 OR ESR-4266 REVISED DECEMBER 17, 2021 RESPECTIVELY.
A. INSTALLATION: INSTALL THE EXPANSION ANCHORS IN ACCORDANCE W/ THE REQUIREMENTS GIVEN IN the icc evaluation report for the specific anchor \& the parameters given in the table BLW.
B. JOB TESTING: FOR VERIFYING SATISFACTORY INSTALLATION WORKMANSHIP, PERFORM JOBSITE TESTING IN ACCORDANCE W/ THE TEST LOAD TABLE PROVIDED UN THIS DOCUMENT. TORQUE TEST 50\% OF THE INSTALLED ANCHORS. ALL TESTS SHALL BE CONDUCTED IN THE PRESENCE OF THE SPECIAL INSPECTOR \& REPORT OF TEST RESULTS SHALL BE SUBMITTED TO HCAI. IF ANY ANCHOR FAILS THE TEST, TEST ALL ANCHORS. THE TEST SHALL BE PERFORMED 24 HOURS OR MORE AFTER INSTALLATION. TESTING MAY BE DONE PRIOR TO EQUIP INSTALLATION, HOWEVER NUT SHALL BE RETORQUED TO INSTALLATION TORQUE AFTER EQUIP INSTALL. ALSO REFER TO CBC 1910A. 5 "TESTS FOR POST-INSTALLED ANCHORS IN CONCRETE". REPORT OF TEST RESULTS SHALL BE SUBMITTED TO HCAI. TESTING SHALL BE PERFORMED BY AN APPROVED TESTING AGENCY EMPLOYED BY THE FACILITY OWNER. TEST REPORTS SHALL BE SUBMITTED TO THE IOR, OWNER \& THE ARCHITECT OR ENGINEER IN RESPONSIBLE CHARGE. (CAC 7-149)
C. FALLURE/ACCEPTANCE CRITERIA: THE FOLLOWING CRITERIA APPLY FOR THE ACCEPTANCE OF INSTALLED ANCHORS:

- TORQUE WRENCH METHOD: THE APPLICABLE TEST TORQUE MUST BE REACHED WITHIN THE FOLLOWING LIMITS:
WEDGE TYPE: ONE-HALF ( $1 / 2$ ) TURN OF THE NUT.
D. AVOID DAMAGING (E) STL REINF IN CONC SLAB WHEN INSTALLING CONC EXPANSION ANCHORS.
E. PROVIDE FOR FULL THRD ENGAGEMENT OF NUT \& WASHER.


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## GENERAL NOTES CONTINUED:

3F. EXPANSION ANCHOR TABLE FOR HILTI KB-TZ \& KB-TZ2 ANCHORS:


| $\qquad$ | ANCHOR DIA (INCH) | INSTALLATION EMBED (INCH) hnom | EFFECTIVE EMBED (INCH) hef | HOLE <br> DEPTH <br> (INCH) <br> ho | MIN CONC THK (INCH) $h$ | MIN CONC EDGE DISTANCE (INCH) | MIN ANCHOR SPCG (INCH) | $\begin{gathered} \text { TEST } \\ \text { TORQUE } \\ \text { (FT-LBS) } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \text { CASE } 1 \\ \text { STRUT R'S } \end{gathered}$ | 3/8 | $13 / 16^{\prime \prime}\left(17 / 8^{\prime \prime}\right)$ | $11 / 2$ | 2 | $31 / 4$ | 6 | 5 | 25 (30) |
| CASE 2 | 1/2 | $23 / 8{ }^{\prime \prime}\left(21 /{ }^{\prime \prime}\right)$ | 2) $R$ | 25/8(23/4) | $C^{4}$ | 12 | $4 / 4$ | 40 (50) |

## NOTES:

1. VALUES IN PARENTHESES ARE FOR HILTI KB-TZ2.
2. VALUES ARE THE SAME FOR bOTH ANCHORS WHERE ONLY ONE NUMBER IS REPORTED.
3. BOLTS THROUGH CONC ON MTL DECK:
A. BOLTS SHALL BE TORQUED BY $3 / 4$ TURN OF-THE NUTS AFTER SNUG TIGHT (THE SNUG TIGHT CONDITION IS DEFINED AS THE TIGHTNESS REQ TO BRING THE CONNECTED PLIES INTO FIRM CONTACT) CONDITION IS ACHIEVED, UNO.
B. THROUGH BOLT HOLES SHALL BE $1 / 16^{\prime \prime}$ LARGER THAN BOLT SIZE (HOLE SIZE $=$ BOLT SIZE $+y_{16}{ }^{n}$ )
C. THROUGH BOLTS IN CONC SHALL RECEIVE SPECIAL INSPECTION \& TESTING (THROUGH BOLTS W/ STL TO STL CONN IN TENSION DO NOT REQUIRE TESTING) IN ACCORDANCE W/ REQUIREMENTS FOR POST-INSTALLED ANCHORS.


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## GENERAL NOTES CONTINUED:

5. TWO (2) CASES OF ANCHORAGE ARE SPECIFIED AND PRESENTED IN THIS PRE-APPROVAL:
 CASE 1: ANCHORAGE DETAILS LOCATED AT UPPER FLOORS ABOVE THE BASE OF A BUILDING ( $\mathrm{z} / \mathrm{h}<=1.0$ ), IT IS ASSUMED THAT THE FLOORS ARE BUILT OF A MIN $3 y_{4}$ " SLWC TOPPING OVER METAL DECK ( $f^{\prime} \mathrm{C}=3000$ PSI, MIN). NOTE THAT CASE 1 MAY ALSO OCCUR AT GRADE OR BLW.
CASE 2: ANCHORAGE DETAILS LOCATED AT OR BELOW THE BASE OF A BUILDING ( $\mathrm{z} / \mathrm{h}=0$ ). THE FLOORS ARE ASSUMED TO BE BUILT OF A MINIMUM 4" NWC SLAB. ( $\mathrm{f}^{\prime} \mathrm{C}=3000 \mathrm{PSI}, \mathrm{MIN}$ ).
6. THIS PRE-APPROVAL MAY BE USED AT ANY GEOGRAPHICAL LOCATION IN THE STATE OF CALIFORNIA. WHERE $\mathrm{S}_{\mathrm{DS}}$ LESS THAN OR EQUAL TO 2.50.


SHEET TITLE: GENERAL NOTES (CONTINUED)

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ABBREVIATIONS:

| AB | ANCHOR BOLT LRFD | LOAD \& RESISTANCE FACTOR DESIGN |
| :---: | :---: | :---: |
| ABV | ABOVE MAX | MAXIMUM |
| ADJ | ADJACENT MFR | MANUFACTURER |
| ASTM | AMERICAN SOCIETY FOR TESTING \& MATERIALS MIN | MINIMUM |
| AWS | AMERICAN WELDING SOCIETY MTL | METAL |
| BD | BECTON, DICKINSON AND COMPANY (N) | NEW |
| BLW | BELOW NO. (\#) | NUMBER OR POUNDS |
| BOTT | BOTTOM NWC | NORMAL WEIGHT CONCRETE |
| CBC | CALIFORNIA BUILDING CODE OD | OUTSIDE DIAMETER |
| CG | CENTER OF GRAVITY OPG | OPENING |
| \& | CENTERLINE PG(S) | PAGE(S) |
| CJP | COMPLETE JOINT PENETRATION ${ }^{\text {P }}$ | PLATE |
| $\mathrm{C}_{\text {max }}$ | MAXIMUM COMPRESSION DUE TO SEISMIC FORCE PSI | POUNDS PER SQUARE INCH |
| CONC | CONCRETE R | RADIUS |
| COORD | COORDINATE REQ | REQUIRED |
| DBL | DOUBLE SEOR | STRUCTURAL ENGINEER OF RECORD |
| DIA ( $\varnothing$ ) | DIAMETER | SAND LIGHT WEIGHT CONCRETE |
| (E) | EXISTING CONDITION SOG | SLAB ON GRADE |
| EA | EACH | SQUARE |
| ELEV | ELEVATION | MAXIMUM TENSION DUE TO SEISMIC FORCE |
| EQUIP | EQUIPMENT < Tu | ANCHORAGE TENSION REACTION DUE TO |
| ES | EACH SIDE | SEISMIC FORCE |
| FF | FINISH FLOOR 4 - | THREAD OR THREADED |
| FLR | FLOOR DE OPIVI-O1 | TOP OF CONCRETE |
| Fp | HORIZONTAL SEISMIC FORCE PER TYP | TYPICAL |
|  | ASCE 7-16 SEISMIC FORCE REQUIREMENTS $\mathrm{mam}_{\text {St }}$ \& $\& \mathrm{Blin}$ | TOP \& BOTTOM |
| FT (') | FOOT/FEET Vu | ANCHORAGE SHEAR REACTION DUE |
| Fv | VERTICAL SEISMIC FORCE PER | TO SEISMIC FORCE |
|  | ASCE 7-16 SEISMIC FORCE REQUIREMENTS | MAXIMUM SHEAR DUE TO SEISMIC FORCE |
| Fy | SPECIFIED YIELD STRENGTH OF REINFORCING, W/ | WITH |
|  | PSI OR SPECIFIED MINIMUM YIELD STRESS Wp | OPERATING WEIGHT |
|  | OF STEEL, KSI No | $\checkmark$ |
| GA | GAUGE |  |
| HCAI | CALIFORNIA DEPARTMENT OF HEALTH |  |
|  | CARE ACCESS AND INFORMATION |  |
| HT | HEIGHT B |  |
| IN (") | INCH |  |
| KSI | KIPS PER SQUARE INCH |  |

SHEET TITLE: ABBREVIATIONS
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## DESIGN CRITERIA:

1. SUPPORT \& ATTACHMENT DESIGN IS PER 2019 CBC AT LRFD LEVEL FORCES.

OTHER MECHANICAL OR ELECTRICAL COMPONENTS PER TABLE 13.6-1 OF ASCE 7-16:
$a_{p}=1.0 \quad R_{p}=1.5 \quad I_{p}=1.5 \quad \Omega_{0}=1.5$ (FOR CONC ANCHORS ONLY)
UPPER FLRS ABV THE BASE OF BLDG
CASE 1: $\quad S_{0 S} \leq 2.50 \quad F_{p}=3.00 \mathrm{~W}_{\mathrm{p}} \quad \mathrm{z} / \mathrm{h} \leq 1.0$
FLRS AT OR BLW THE BASE OF BLDG
CASE 2: $\quad \mathrm{S}_{\mathrm{DS}} \leq 2.5$
$F_{p}=1.125 W_{p} \quad z / h=0$
LOAD COMBINATIONS

$$
\begin{aligned}
& \left(0.9-0.2 \mathrm{~S}_{\mathrm{DS}}\right) D-\Omega_{0} F_{\mathrm{p}} \text { (FOR MAX TENSION) } \\
& \left(1.2+0.2 \mathrm{~S}_{\mathrm{DS}}\right) D+\Omega_{0} F_{\mathrm{p}} \text { (FOR MAX COMPRESSION) }
\end{aligned}
$$

2. THIS PRE-APPROVAL MAY BE USED ONLY AT GEOGRAPHICAL LOCATIONS IN THE STATE OF CALIFORNIA WHERE $S_{D S} \& z / h$ COMPLY W/ VALUES SHOWN ABOVE. OTHER COMBINATIONS OF $S_{D S} \& z / h$ ARE ACCEPTABLE PROVIDED THAT SEOR DEMONSTRATES THAT THE CORRESPONDING Fp VALUE IS LESS THAN OR EQ TO VALUE SHOWN ABV.



## NOTES:

1. FOR CASE 1 \& CASE 2 ANCHORAGE TO FLR, SEE PGS 11 TO 13.
2. BRACKET LAYOUT SHALL BE FOLLOWED AS SHOWN ON PLANS ON PG 7.

| BD INTEGRATED DIAGNOSTIC SOLUTIONS TOTALYS MULTIPROCESSOR |  |  |  |
| :---: | :---: | :---: | :---: |
| NOTES: <br> 1. FOR CASE 1 \& CASE 2 ANCHORAGE TO FLR, SEE PGS 11 TO 13. <br> 2. BRACKET LAYOUT SHALL BE FOLLOWED AS SHOWN ON PLANS ON PG 7. |  |  |  |
|  |  |  |  |
| SHEET TITLE: SEISMIC BRACKET ASSEMBLY DETAIL |  |  |  |
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## NOTE:

DUE TO TIGHT TOLERANCE, TAKE EXTREME CARE WHEN LAYING OUT LOCATIONS FOR CONC AB.


SHEET TITLE: BRACKET "A" DETAIL
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SHEET TITLE: BRACKET "B" DETAIL

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OVERSTRENGTH FACTOR ( $\Omega_{0}$ ) INCLUDED.



